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A spray powder for the manufacture of a thermally insulating layer which remains resistant at high temperatures.

### SUBSTITUTE SPECIFICATION

#### SPRAY POWDER FOR THE MANUFACTURE OF A THERMALLY INSULATING LAYER WHICH REMAINS RESISTANT AT HIGH TEMPERATURES

##### Background of the Invention

**[0001]** The invention relates to a spray powder for the manufacture of a thermally insulating layer which remains resistant to high temperatures ~~in accordance with the preamble of claim 1.~~ It relates to a method for the manufacture of the spray powder in accordance with the invention and also to a substrate coated by means of a thermal spraying process and using the spray powder in accordance with the invention. The substrate is a substance from which, for example, the blade of a gas turbine wheel is made.

**[0002]** A thermally insulating layer of this kind is termed TBC ("thermal barrier coating". The substrate onto which the TBC is sprayed, can already be coated with a single ~~or multilayered~~ multi-layered partial coating, in particular a primer. A least one thermally insulating functional material is used as a coating material, which on the one hand has a strikingly lower thermal conductivity than the substrate and, on the other hand, forms a chemically and thermally stable phase at high temperatures.

**[0003]** Characteristics of a coating of the type TBC, its possible material composition and also problems relating to the ageing of this coating are known from EP-A- 1 225 251. In this publication the main emphasis is

laid-on coatings with columnar microstructures, which can be manufactured by means of processes in which the functional material - advantageously YSZ (zirconium oxide, which is ~~stabilised~~stabilized with yttrium) - is ~~vaperised~~vaporized and condensed out on the surface to be coated. Such processes are PVD or sputter processes for example. Non - columnar coatings, which are likewise discussed in ~~EPA~~EP-A 1 225 251, result during thermal spraying processes using suitable powder mixtures. During thermal spraying processes an anisotropic, inhomogeneous microstructure is formed with granules, at the boundaries of which micro-pores occur, in particular also gap-shaped micro-pores.

The ~~[0004]~~ EP-A- 1-25- 225 251 mentions the ageing of the coatings: ~~the~~The relatively low thermal insulation of the TBC is concerned with inhomogeneities of the microstructure, which is given by a plurality of crystal granules, wherein the boundary zones between the granules are decisive. The local density is less in these boundary zones than inside the crystals. The micro-pores and lattice defects inside the granules also have a lowering effect on the thermal conductivity. As regards the ageing processes, these are thickenings of the microstructure, which result at high temperatures due to a sintering together—, namely a ~~homogenising~~homogenizing growing together of micro-pores at the granule boundaries. The thermal conductivity, which should remain as low as possible, increases with higher compression. Contaminants which are present due to silicon, titanium, iron, nickel, sodium, lithium, copper, manganese, potassium and /or oxides of some of these elements, result in amorphous phases, which form thin films at the granule boundaries. Amorphous phases of this kind encourage the ~~homogenisation~~homogenization of the coating on the basis of a sintering together of the granules. The ~~homogenisation~~homogenization processes can be eliminated, prevented or at least slowed down with suitable additives. An additive of this kind is ~~aluminium~~aluminum oxide, which is present in the

form of precipitated crystallites. These can bind the named contaminants and in addition fix the micro-pores which are located between the granules. The ~~aluminium~~aluminum oxide absorbs silicates out of the films, which bind the ~~neighbouring~~neighboring granules. Thus gap-like empty cavities form between the ~~neighbouring~~neighboring granules which represent barriers for a transport of heat.

### Summary of the Invention

The [0005] It is an object of the invention ~~is to~~ create a spray powder for a coating of the TBC type, whose inhomogeneity, which stands in relation to the thermal conductivity, is particularly strongly pronounced and thermally durable. ~~This object is satisfied by the spray powder defined in claim 1.~~

[0006] The spray powder can be used for the manufacture of a thermally insulating layer which is stable at high temperatures. This TBC can be produced on a substrate by means of a thermal spraying process. The substrate can already be coated with ~~single~~ or ~~multilayer~~multi-layer part coating, in particular a primer. At least one thermally insulating functional material is used, which on the one hand has a lower thermal conductivity than the substrate and on the other hand forms a chemically and thermally stable phase at high temperatures. The spray powder comprises particles, which respectively have an agglomerate-like micro-structure, which is formed by a plurality of granules adhering to each other. These granules are made of the functional material or the functional materials. At least one further component made of an additive or a plurality of additives is present. This further component is distributed finely dispersed on the surfaces of the functional material granules, i.e. mainly in their boundary zones. In the given form or in a transformed form, the further components exert a retarding or eliminating effect with regard to sintering compounds, which can form at high temperatures between the functional material granules. The spray powder in accordance with the invention has specifically manufactured micro-structures of its particles. These micro-structures are

maintained, at least partially, during coating by means of thermal spraying and thus lead to a strongly pronounced inhomogeneity, which is accompanied by a lower thermal conductivity. This inhomogeneity has the required durability ~~thanks due~~ to suitable additives or ~~thanks due~~ to materials, which have resulted from a transformation from the additives.

~~The dependent claims 2 to 6 relate to advantageous embodiments of the spray powder in accordance with the invention. Methods for the manufacture of the spray powder in accordance with the invention are the subject of claims 7 to 9. Claim 10 relates to a coated substrate with a TBC.~~

**[0007]** The invention will be explained in the following on the basis of the drawings. ~~They show:~~

#### Brief Description of the Drawings

**[0008]** Fig. 1 is an illustration of the micro-structure, which a particle of the spray powder has in accordance with the invention ~~has~~, and

**[0009]** Fig. 2 is a schematic illustration of a whole particle.

#### Description of the Preferred Embodiments

**[0010]** The spray powder in accordance with the invention consists of particles 1 or comprises these. The particles 1 have respectively an agglomerate-like micro-structure 2, as illustrated in ~~Figure~~Fig. 1. ~~Figure~~Fig. 2 shows a schematic illustration of a cross-section through a whole particle 1, which has a boundary zone 10 between two areas 11 and 12 marked with chain dotted lines. In this arrangement the area 11 is the surface of the particle 1. The micro-structure 2 is indicated at a point in the interior of the particle 1. The particle 1 is made up of a plurality of granules 3 adhering to each other. At the surfaces 30 of the granules 3, where they are in contact with ~~neighbouring~~neighboring granules, micro-pores produce low mass boundary zones 5. Lattice defects, impurity ions and/or further micro-pores

(not illustrated) contribute to the reduction of the thermal conductivity inside the granules 3, which can also be polycrystalline.

**[0011]** Each granule 3 consists of one functional material, the function of which is to keep a flow of heat through this functional material granule 3 low at high temperatures. Different functional materials can also be present. At least one additive 4 forms a further component of the particle 1. This further component is distributed finely dispersed on the surfaces 30 of the functional material granules 3, i.e. mainly in their boundary zones 5. It exerts - if necessary after a transformation into another form - a retarding or eliminating effect with regard to ~~homogenising~~homogenizing sintering effects, which occur, or can occur, at high temperatures on the surfaces of the functional material granules 3. With regard to the named transformation of the additive 4, this can initially be melted and form a new phase, together with material from ~~neighbouring~~neighboring functional material granules 3. The new phase co-exists with the phase of the functional material granules 3. The effect of the additive 4 which influences the sintering process is explained in EP-A- 1 225 251.

**[0012]** It is also possible to incorporate the additive 4 in the particle 1 in a form which is first transformed into an effective form by means of an additional treatment. The additives 4 can be deposited in a phase consisting of metal salts, wherein these salts can be transformed thermally into metal oxides. Only after a transformation of the salts by means of a thermal treatment step do the additives 4 assume the effective form, namely the form which influences the sintering process.

**[0013]** In relation to all the components, the component which is formed from the additive 4 or the additives, has a proportion of not more than 5 mol %, preferably 3 mol % at the most. The functional material granules 3 have an average diameter  $d_{50}$  greater than 1nm and smaller than 10 $\mu$ m, while the particles 1 of the spray powder have an average diameter  $d_{50}$  in the

range from 1 to 100  $\mu\text{m}$  (50% by weight of the granules 3 or particles 1 are larger - or smaller - than the corresponding diameter  $d_{50}$ ). The particle diameter  $d_{50}$  is preferably in the range of 40 to 90  $\mu\text{m}$  for plasma spraying processes, which are normally used. The preferred range can also be different for other processes, for example between 5 and 25  $\mu\text{m}$ .

**[0014]** The particles 1 of the spray powder are porous agglomerates of the functional material granules 3, which contain respectively communicating, open pore cavities open towards the outer surface 11 of the particle 1, namely the boundary zones 5. The additives 4 can be stored in these pore cavities 5 or deposited on the outer surface 11 of the particle 1.

**[0015]** The functional material described in EP-A- 1 225-231 251 is zirconium oxide, in particular the ~~stabilised~~stabilized zirconium oxide YSZ. This is a particularly advantageous material. Others are also possible however.

**[0016]** A ceramic material with a pyrochloic structure, for example lanthanum zirconate, can be used as a functional material (see US-A- ~~6,117,560~~, patent 6,117,560, Maloney). The pyrochloic structure is specifically expressed by the formula  $A_2B_2O_7$ , wherein A and B are elements which are present in a cationic form  $A^{n+}$  and  $B^{m+}$  respectively and for which the pair of values  $(n, m) = (3, 4)$  or  $(2, 5)$  apply for their charges  $n+$  and  $m+$ . More generally the formula for the pyrochloic structure is  $A_{2-x}B_{2+x}O_{7-y}$ , wherein x and y are positive numbers, which are small compared with 1. The following chemical elements may be selected for A and B: A = La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb or a mixture of these chemical elements and B = Zr, Hf, Ti.

**[0017]** A further possible functional material is a magnetoplumbite phase (see WO 99/42630, Gadow):  $MMeAl_{11}O_{19}$ , M = La, Nd and Me = Mg, Zn, Co, Mn, Fe, Ni, Cr.

**[0018]** For example an Al-, Mg- or La-oxide can be employed as an additive 4, further a yttrium ~~aluminium~~aluminum oxide (see US-A-~~6203927~~, patent 6,203,927, Subramanian et al.) or also a spinel, in particular magnesium ~~aluminium~~aluminum oxide. The following steps can be taken to incorporate the additive 4 between the functional granules 3 for example. On the one hand particle-shaped agglomerates of the functional granules 3 are manufactured and on the other hand a metal salts solution is prepared from dissolved Al-, Mg-, La-nitrate or from the corresponding acetate. The agglomerate particles are impregnated with the solution and the impregnated particles are dried. This impregnation can be repeated. A transformation into oxides, which represent the effective additives, occurs by means of a thermal treatment of the named nitrate or acetate salts. The agglomerates are won by spray drying of slurries of the functional granules 3 and subsequent sintering (calcining) of the dried intermediate product.

**[0019]** Each additive 4, or its modified form, effectively influencing the sintering process ~~can not~~cannot be miscible with the functional material, so that a diffusion into the functional material is largely prevented.

**[0020]** A method for the manufacture of the spray powder in accordance with the invention has already been described essentially. There are also alternatives, namely an alternative A2 in addition to the A1 described:

A1) At least one of the additives 4 is introduced into a porous agglomerate of the functional material granules 3 by means of a impregnation process.

A2) The agglomerates are manufactured from a mixture of functional material granules 3 and finely dispersed additive 4, wherein the agglomerates are preferably produced by ~~the~~forming and spray drying of a slurry ~~(forming of a slurry)~~ and subsequent calcination. The additive 4, for example nitrate, chloride or acetate salt, can also be introduced into the

slurry in solution. Instead of a solution, a suspension is also possible, in which the additive 4 is dispersed in colloidal form.

**[0021]** In a concluding advantageous method step the agglomerates are introduced into a plasma flame for a short time and thus partially melted. If necessary the components can at least partially result from a thermal transformation out of the additive which brings about the inhibiting of the sintering process. Moreover a mechanically tougher form of the powder particles 1 is formed, for the reason that a partially sintered edge layer 10 occurs.